

UNIT IV

STABILITY ANALYSIS

Numerical Integration methods

- Modified Euler's method
- Runge-Kutta method

MODIFIED EULER'S METHOD

- Using first derivative of the initial point next point is obtained
- $X_1^p = X_0 + \frac{dX}{dt} \Delta t$ the step $t_1 = t_0 + \Delta t$
- Using this x_1^p $\frac{dx}{dt}$ at $x_1^p = f(t_1, x_1^p)$

MODIFIED EULER'S METHOD

- Corrected value is

$$X_1^P = X_0 + \left\{ \frac{\left(\frac{dx}{dt} \right)_{X_0} + \left(\frac{dx}{dt} \right)_{X_1^P}}{2} \right\} \Delta t$$

$$X_{i+1}^c = X_i + \left\{ \frac{\left(\frac{dx}{dt} \right)_{X_i} + \left(\frac{dx}{dt} \right)_{X_{i-1}^P}}{2} \right\} \Delta t$$

Numerical Solution of the swing equation

- Input power $p_m = \text{constant}$

- At steady state $p_e = p_m$,

$$\delta_0 = \sin^{-1} \left(\frac{P_m}{P_{1\max}} \right)$$

$$P_{1\max} = \frac{|E'| |V|}{X_1}$$

- At synchronous speed $\Delta\omega_0 = 0$

$$P_{2\max} = \frac{|E'| |V|}{X_2}$$

The swing equation

$$\frac{H}{\pi f_0} \frac{d^2\delta}{dt^2} = p_a = (p_m) - p_e$$

$$\frac{d^2\delta}{dt^2} = \frac{\pi f_0}{H} (p_m - p_{2\max} \sin \delta) = \frac{\pi f_0}{H} p_a$$

$$\frac{d\delta}{dt} = \Delta\omega$$

$$\frac{d\Delta\omega}{dt} = \frac{\pi f_0}{H} p_a = \frac{d^2\delta}{dt^2}$$

Applying Modified Eulers method to above equation

$$t_1 = t_0 + \Delta t$$

$$\delta_{i+1}^p = \delta_i + \left(\frac{d\delta}{dt} \right)_{\Delta\omega_i} \Delta t$$

$$\Delta\omega_{i+1}^p = \Delta\omega_i + \left(\frac{d\Delta\omega}{dt} \right)_{\delta_i} \Delta t$$

- The derivatives at the end of interval

$$\left(\frac{d\delta}{dt} \right)_{\Delta\omega_{i+1}^p} = \Delta\omega_{i+1}^p$$

$$\left(\frac{d\Delta\omega}{dt} \right)_{\delta_{i+1}^p} = \left(\frac{\pi f_0}{H} p_a \right)_{\delta_{i+1}^p}$$

The corrected value

$$\delta_{i+1}^c = \delta_i + \left(\frac{\left(\frac{d\delta}{dt} \right)_{\Delta\omega_i} + \left(\frac{d\delta}{dt} \right)_{\Delta\omega_{i+1}^p}}{2} \right) \Delta t$$

$$\Delta\omega_{i+1}^c = \Delta\omega_i + \left(\frac{\left(\frac{d\Delta\omega}{dt} \right)_{\delta_i} + \left(\frac{d\Delta\omega}{dt} \right)_{\delta_{i+1}^p}}{2} \right) \Delta t$$

Runge-Kutta Method

- Obtain a load flow solution for pretransient conditions
- Calculate the generator internal voltages behind transient reactance.
- Assume the occurrence of a fault and calculate the reduced admittance matrix
- Initialize time count $K=0, J=0$

Runge-Kutta Method

- Determine the eight constants

$$K_1^k = f_1(\delta^k, \omega^k) \Delta t$$

$$l_1^k = f_2(\delta^k, \omega^k) \Delta t$$

$$K_2^k = f_1\left(\delta^k + \frac{K_1^k}{2}, \omega^k + \frac{l_1^k}{2}\right) \Delta t$$

$$l_2^k = f_2\left(\delta^k + \frac{K_1^k}{2}, \omega^k + \frac{l_1^k}{2}\right) \Delta t$$

$$K_3^k = f_1\left(\delta^k + \frac{K_2^k}{2}, \omega^k + \frac{l_2^k}{2}\right) \Delta t$$

$$l_3^k = f_2\left(\delta^k + \frac{K_2^k}{2}, \omega^k + \frac{l_2^k}{2}\right) \Delta t$$

$$K_4^k = f_1\left(\delta^k + \frac{K_3^k}{2}, \omega^k + \frac{l_3^k}{2}\right) \Delta t$$

$$l_4^k = f_2\left(\delta^k + \frac{K_3^k}{2}, \omega^k + \frac{l_3^k}{2}\right) \Delta t$$

$$\Delta \delta^k = \frac{\left(K_1^k + 2K_2^k + 2K_3^k + K_4^k\right)}{6}$$

$$\Delta \omega^k = \frac{\left(l_1^k + 2l_2^k + 2l_3^k + l_4^k\right)}{6}$$

Compute the change in state vector

$$\Delta \delta^k = \frac{(K_1^k + 2K_2^k + 2K_3^k + K_4^k)}{6}$$

$$\Delta \omega^k = \frac{(l_1^k + 2l_2^k + 2l_3^k + l_4^k)}{6}$$

Evaluate the new state vector

$$\delta^{k+1} = \delta^k + \Delta \delta^k$$

$$\omega^{k+1} = \omega^k + \Delta \omega^k$$

Evaluate the internal voltage behind transient reactance using the relation

$$E_p^{k+1} = |E_p^k| \cos \delta_p^{k+1} + j |E_p^k| \sin \delta_p^{k+1}$$

Check if $t < t_c$ yes $K = K + 1$

Check if $j = 0$, yes modify the network data and obtain the new reduced

admittance matrix and set $j = j + 1$

set $K = K + 1$

Check if $K < K_{\max}$, yes start from finding 8 constants

Thank you